

**NASA TECHNICAL
MEMORANDUM**



N73-29600
NASA TM X-2875

NASA TM X-2875

**CASE FILE
COPY**

**IMPROVING THE ACCURACY
OF ANGULAR-MOMENTUM PROJECTION**

by William F. Ford

*Lewis Research Center
Cleveland, Ohio 44135*

1. Report No. NASA TM X-2875		2. Government Accession No.		3. Recipient's Catalog No.	
4. Title and Subtitle IMPROVING THE ACCURACY OF ANGULAR-MOMENTUM PROJECTION				5. Report Date August 1973	
				6. Performing Organization Code	
7. Author(s) William F. Ford				8. Performing Organization Report No. E-7483	
9. Performing Organization Name and Address Lewis Research Center National Aeronautics and Space Administration Cleveland, Ohio 44135				10. Work Unit No. 503-10	
				11. Contract or Grant No.	
12. Sponsoring Agency Name and Address National Aeronautics and Space Administration Washington, D.C. 20546				13. Type of Report and Period Covered Technical Memorandum	
				14. Sponsoring Agency Code	
15. Supplementary Notes					
16. Abstract <p>A connection is established between Ullah's new method of angular-momentum projection and the conventional Hill-Wheeler method. They are studied for the case where series truncation of some sort is required. It is shown that for a particular choice of angles the analysis simplifies greatly and at the same time leads to reduced truncation error.</p>					
17. Key Words (Suggested by Author(s)) Nuclear physics Rotational nuclei Angular-momentum projection				18. Distribution Statement Unclassified - unlimited	
19. Security Classif. (of this report) Unclassified		20. Security Classif. (of this page) Unclassified		21. No. of Pages 9	
				22. Price* \$3.00	

* For sale by the National Technical Information Service, Springfield, Virginia 22151

Page Intentionally Left Blank

IMPROVING THE ACCURACY OF ANGULAR-MOMENTUM PROJECTION

by William F. Ford

Lewis Research Center

SUMMARY

A connection is established between Ullah's new method of angular-momentum projection and the conventional Hill-Wheeler method. They are studied for the case where series truncation of some sort is required. It is shown that for a particular choice of angles the analysis simplifies greatly and at the same time leads to reduced truncation error.

INTRODUCTION

Recently Ullah proposed a new method (ref. 1) for performing angular-momentum projection, designed to avoid the difficulties associated with numerical integration of rapidly oscillating rotation matrices. Considering the case of axially symmetric intrinsic wave functions Φ_K , he used Löwdin's representation (ref. 2) of the projection operator P_{JK} to write

$$\begin{aligned}\Omega_J &\equiv \langle \Phi_K | \Omega P_{JK} | \Phi_K \rangle \\ &= (2J + 1) \frac{(J + K)!}{(J - K)!} \sum_{n=0}^{J_{\max} - J} (-1)^n \frac{C_{J-K+n}}{n!(2J + n + 1)!}\end{aligned}\quad (1)$$

where Ω is some rotationally invariant operator (usually H or 1) and

$$C_n = \langle \Phi_K | \Omega J_-^n J_+^n | \Phi_K \rangle \quad (2)$$

(Both Ω_J and C_n depend on K , but for simplicity this dependence will be left implicit.) Rather than evaluate equation (2) directly, Ullah showed that the coefficients C_n could be found by means of a generating function

$$\left\langle \Phi_K \left| \Omega e^{\lambda J_-} e^{-\lambda J_+} \right| \Phi_K \right\rangle = \sum_{n=0}^N (-1)^n \frac{\lambda^{2n}}{(n!)^2} C_n \quad N \equiv J_{\max} - K \quad (3)$$

and then devised an elegant transformation to reduce the left side to

$$(1 - \lambda^2)^{-K} \left\langle \Phi_K \left| \Omega e^{-i\beta J_y} \right| \Phi_K \right\rangle \quad (4)$$

where

$$\sin\left(\frac{1}{2}\beta\right) = \lambda$$

If equation (3) is considered for a set of $N + 1$ different values of λ , a simple matrix inversion (ref. 3) will yield the coefficients C_n .

CONNECTION WITH HARMONIC ANALYSIS METHOD

Basically, Ullah's method is an improvement of one developed previously by Mihailovic, Kuhawski, and Lesjak (ref. 4). Working from an expression which can be written (for rotationally invariant operators) in our notation as

$$\left\langle \Phi_K \left| e^{\theta J_-} \Omega e^{\theta J_+} \right| \Phi_K \right\rangle = \sum_{n=0}^N \frac{C'_n}{(n!)^2} \theta^{2n} \quad N = J_{\max} - K \quad (5)$$

they obtain the coefficients C'_n by means of harmonic analysis and then numerically solve the set of linear equations

$$C'_n = \sum_{J=K+n}^{J_{\max}} \frac{(J+K+n)!(J-K)!}{(J-K-n)!(J+K)!} \Omega_J \quad (6)$$

to find the desired quantities Ω_J . This is unnecessarily cumbersome, however, since by writing

$$C'_{L-K+n} = \sum_{J=L+n}^{J_{\max}} \frac{(J+L+n)!(J-K)!}{(J-L-n)!(J+K)!} \Omega_J \quad (7)$$

and using the identity

$$(2L+1) \sum_{n=0}^{J-L} \frac{(J+L+n)!}{(J-L-n)!} \frac{(-1)^n}{n!(2L+n+1)!} = \delta_{LJ} \quad (8)$$

we may easily solve the linear equations analytically, obtaining

$$\Omega_L = (2L+1) \frac{(L+K)!}{(L-K)!} \sum_{n=0}^{J_{\max}-L} \frac{(-1)^n}{n!(2L+n+1)!} C'_{L-K+n} \quad (9)$$

the form proposed by Ullah. The identity (8) may be established by noting that the left side is proportional to the hypergeometric function ${}_2F_1(L+J+1, L-J; 2L+2; 1)$. This in turn may be written in closed form, and the left side reduces to $(2L+1)/(L+J+1)(L-J)!(J-L)!$

Another difficulty is that the transformation used by Mihailovic, Kujawski, and Lesjak to render their equations harmonic requires evaluation of equation (5) at $2N+1$ different complex values of θ to obtain the $N+1$ coefficients C'_n . Since calculation of the overlap integral in equation (5) is difficult and lengthy on even the fastest computers, the direct method proposed by Ullah, which requires only $N+1$ different evaluations, is to be preferred.

There still remains a problem, however. If the dimensionality of the model space used to define Φ_K is allowed to increase, or an "inert" core is allowed to become "active", the value of J_{\max} can become enormous. In that case the expansion (3) must be truncated for practical reasons, and it is not clear how to choose the set of λ values so as to minimize the truncation error.

CONNECTION WITH HILL-WHEELER METHOD

It is instructive to compare Ullah's method with the conventional one employing the Hill-Wheeler integral (ref. 5),

$$\Omega_J = \frac{2J+1}{2} \int_0^\pi \langle \Phi_K | \Omega e^{-i\beta J_y} | \Phi_K \rangle d_{KK}^J(\beta) \sin \beta d\beta \quad (10)$$

where

$$d_{KK}^J(\beta) \equiv \langle JK | e^{-i\beta J_y} | JK \rangle$$

is an element of the reduced rotation matrix. It has been pointed out by Ripka (ref. 6) that direct numerical integration of equation (10) is likely to be inaccurate for large values of J , because of the rapid oscillations of $d_{KK}^J(\beta)$. The factor $\langle \Phi_K | \Omega \exp(-i\beta J_y) | \Phi_K \rangle$, on the other hand, is relatively smooth except for a strong peak at $\beta = 0$ (and possibly at $\beta = \pi$) (refs. 7 and 8). This suggests an expansion in powers of some suitable function of β , and from Ullah's work (see eqs. (3) and (4)) it is apparent that one such expansion, with only a finite number of terms, is

$$\langle \Phi_K | \Omega e^{-i\beta J_y} | \Phi_K \rangle = \left(\cos \frac{1}{2} \beta \right)^{2K} \sum_{n=0}^N (-1)^n \frac{C_n}{(n!)^2} \left(\sin \frac{1}{2} \beta \right)^{2n} \quad (11)$$

Using equation (11) in (10) results in

$$\Omega_J = \frac{2J+1}{2} \sum_{n=0}^N C_n Q_n^{JK} \quad (12)$$

where

$$\begin{aligned} Q_n^{JK} &= \frac{(-1)^n}{(n!)^2} \int_0^\pi \left(\sin \frac{1}{2} \beta \right)^{2n} \left(\cos \frac{1}{2} \beta \right)^{2K} d_{KK}^J(\beta) \sin \beta d\beta \\ &= \frac{(-1)^n}{(n!)^2} \int_{-1}^1 \left(\frac{1-x}{2} \right)^n \left(\frac{1+x}{2} \right)^{2K} P_{J-K}^{(0, 2K)}(x) dx \end{aligned} \quad (13)$$

Here the reduced rotation matrix has been replaced by its representation in terms of a Jacobi polynomial (ref. 9). Because of the orthogonality property of Jacobi polynomials, the integral in equation (13) vanishes unless $n \geq J - K$. Its nonvanishing values are

given by (ref. 10)

$$Q_{J-K+n}^{JK} = 2(-1)^n \frac{(J+K)!}{(J-K)!} \frac{1}{n!(2J+n+1)!} \quad (14)$$

and we recover Ullah's result.

A SIMPLIFIED METHOD BASED ON ORTHOGONAL POLYNOMIALS

The previous section illustrates the connection between Ullah's expansion and the conventional Hill-Wheeler integral treatment. The orthogonality feature, however, suggests a different expansion of the integrand factor in equation (10), namely, that the terms in equation (11) be rearranged so that

$$\begin{aligned} \langle \Phi_K | \Omega e^{-i\beta J_y} | \Phi_K \rangle &= \left(\cos \frac{1}{2} \beta \right)^{2K} \sum_{J=K}^{J_{\max}} a_J P_{J-K}^{(0, 2K)}(\cos \beta) \\ &= \sum_{J=K}^{J_{\max}} a_J d_{KK}^J(\beta) \end{aligned} \quad (15)$$

We then obtain the remarkably simple result

$$\Omega_J = \langle \Phi_K | \Omega P_{JK} | \Phi_K \rangle = a_J \quad (16)$$

Of course, this is really not so surprising, since equations (10) and (15) together form a statement of the expansion theorem for orthogonal functions, that is, one implies the other. The importance of equation (15), however, is not only that its coefficients $a_J = \Omega_J$ may be obtained by exactly the same procedure suggested by Ullah, namely, matrix inversion, but in addition that for a particular choice of angles it is possible to arrange matters so that the matrix inversion can be done trivially and yet furnish a superior approximation to the integral if the expansion is truncated at $J = J_0$.

This is accomplished by using the roots β_n of the first neglected rotation matrix

$$d_{KK}^{J_0+1}(\beta_n) = 0 \quad n = 0, 1, \dots, N_0 = J_0 - K \quad (17)$$

(excluding the $2K$ -multiple root $\beta = \pi$), because for these angles the Christoffel-Darboux

formula (ref. 11) for Jacobi polynomials yields an "orthogonality" relation:

$$\sum_{J=K}^{J_0} \left(\frac{2J+1}{2} \right) d_{KK}^J(\beta_m) d_{KK}^J(\beta_n) = 0 \quad m \neq n \quad (18)$$

With this relation the $N_0 + 1$ linear equations obtained by setting $\beta = \beta_n$ in equation (15) are easily solved, yielding

$$\Omega_J = \sum_{n=0}^{N_0} w_n \left[\left(\frac{2J+1}{2} \right) d_{KK}^J(\beta_n) \left\langle \Phi_K \left| \Omega e^{-i\beta_n J y} \right| \Phi_K \right\rangle \right] \quad (19)$$

where

$$w_n = \left[\sum_{J=K}^{J_0} \left(\frac{2J+1}{2} \right) d_{KK}^J(\beta_n)^2 \right]^{-1} \quad (20)$$

Since the Christoffel-Darboux formula is of the form

$$\sum_n^N C_n P_n(x) P_n(y) = \frac{F_n(x, y)}{y - x}$$

it follows that if $y = x + \epsilon$ with $\epsilon \rightarrow 0$, then

$$\sum_n^N C_n P_n(x)^2 = \frac{\partial F_N}{\partial y} \bigg|_{y=x}$$

This may be used to sum the series in equation (20), with the result

$$w_n = 2 \left[\frac{(J_0 + 1) \sin \beta_n}{(J_0 + 1 + K)(J_0 + 1 - K) d_{KK}^{J_0}(\beta_n)} \right]^2 \quad (21)$$

These formulas have the appearance of an algorithm for the numerical integration of equation (10) and in fact are identical to those which would be obtained from a Gauss

quadrature method of order N_0 based on the orthogonal functions $d_{KK}^J(\beta)$. As such, they are known to be exact if the integrand can be expressed in terms of the first $2N_0 + 1$ such functions. We conclude that, if the expansion (15) is terminated at $J = J_0$ and its coefficients are determined by equation (19), truncation error will affect only those Ω_J for which $J > 2J_0 + 1 - J_{\max}$; those with $J \leq 2J_0 + 1 - J_{\max}$ will remain exact. The magnitude of the truncation error is difficult to estimate, but the Gauss method is known to be remarkably accurate.

CONCLUDING REMARK

One caveat should be sounded: if the dimensionality or number of nucleons is large, the number of terms which can be taken is severely limited by the computing time required to evaluate $\langle \Phi_K | \Omega \exp(-i\beta J_y) | \Omega_K \rangle$. At the same time, the behavior of the integrand places a greater burden of accuracy on the series expansion. In a typical calculation for ^{20}Ne , for instance, with all nucleons active and states up to $1g_{9/2}$ included, the left side of equation (15) falls from 1.00 at $\beta = 0^\circ$ to 0.070 at $\beta = 45^\circ$ to 0.001 at $\beta = 65^\circ$. Here the strong forward peaking is of more concern than oscillations of $d_{KK}^J(\beta)$, and it may be profitable to consider a transformation on the variable of integration before attempting numerical procedures. In that event it would probable be best to treat the transformed integrand by means of a Gauss quadrature based on Chevyshev polynomials, because of the ease in calculating weights and abscissas.

Lewis Research Center,
National Aeronautics and Space Administration,
Cleveland, Ohio, July 2, 1973,
503-10.

REFERENCES

1. Ullah, Nazaket: New Method for the Angular-Momentum Projection. Phys. Rev. Letters, vol. 27, no. 7, Aug. 16, 1971, pp. 439-442.
2. Löwdin, Per-Olov: Angular Momentum Wavefunctions Constructed by Projection Operators. Rev. Mod. Phys., vol. 36, no. 4, Oct. 1964, pp. 966-976.
3. Burnside, William S.; and Panton, A. W.: The Theory of Equations. Vol. II. Dover Publ., 1960.

4. Mihailovic, M. V.; Kujawski, E.; and Lesjak, J.: Projection of Angular Momentum and the Generator Coordinate Method for Light Nuclei. Nucl. Phys., vol. A161, 1971, pp. 252-262.
5. Hill, David L.; and Wheeler, John A.: Nuclear Constitution and the Interpretation of Fission Phenomena. Phys. Rev., vol. 89, no. 5, Mar. 1, 1953, pp. 1102-1145.
6. Ripka, G.: Lectures in Theoretical Physics. P. D. Kunz, et al., eds., Univ. Colorado Press, 1966, p. 237.
7. Villars, F.: Proceedings of the International School of Physics Enrico Fermi. Course XXXVI. Academic Press, 1966, p. 26.
8. Warke, Chindhu S.; and Gunye, M. R.: Properties of the Projected Spectra for Finite Nuclei. Phys. Rev., vol. 155, no. 4, Mar. 20, 1967, pp. 1084-1089.
9. Edmonds, A. R.: Angular Momentum in Quantum Mechanics. Princeton Univ. Press, 1957, p. 58.
10. Erdélyi, A., ed.: Tables of Integral Transforms. McGraw-Hill Book Co., Inc., 1954, Vol. II, Sec. 16.4.
11. Abramowitz, Milton; and Stegun, Irene A., eds.: Handbook of Mathematical Functions with Formulas, Graphs, and Mathematical Tables. Appl. Math. Ser. 55, National Bureau of Standards, June 1964, Ch. 22.



POSTMASTER: If Undeliverable (Section 158
Postal Manual) Do Not Return

"The aeronautical and space activities of the United States shall be conducted so as to contribute . . . to the expansion of human knowledge of phenomena in the atmosphere and space. The Administration shall provide for the widest practicable and appropriate dissemination of information concerning its activities and the results thereof."

—NATIONAL AERONAUTICS AND SPACE ACT OF 1958

NASA SCIENTIFIC AND TECHNICAL PUBLICATIONS

TECHNICAL REPORTS: Scientific and technical information considered important, complete, and a lasting contribution to existing knowledge.

TECHNICAL NOTES: Information less broad in scope but nevertheless of importance as a contribution to existing knowledge.

TECHNICAL MEMORANDUMS: Information receiving limited distribution because of preliminary data, security classification, or other reasons. Also includes conference proceedings with either limited or unlimited distribution.

CONTRACTOR REPORTS: Scientific and technical information generated under a NASA contract or grant and considered an important contribution to existing knowledge.

TECHNICAL TRANSLATIONS: Information published in a foreign language considered to merit NASA distribution in English.

SPECIAL PUBLICATIONS: Information derived from or of value to NASA activities. Publications include final reports of major projects, monographs, data compilations, handbooks, sourcebooks, and special bibliographies.

TECHNOLOGY UTILIZATION PUBLICATIONS: Information on technology used by NASA that may be of particular interest in commercial and other non-aerospace applications. Publications include Tech Briefs, Technology Utilization Reports and Technology Surveys.

Details on the availability of these publications may be obtained from:

SCIENTIFIC AND TECHNICAL INFORMATION OFFICE

NATIONAL AERONAUTICS AND SPACE ADMINISTRATION
Washington, D.C. 20546